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(56) Documents Cited

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| US 4251133 A | US 4241983 A | US 4240703 A |
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(58) Field of Search

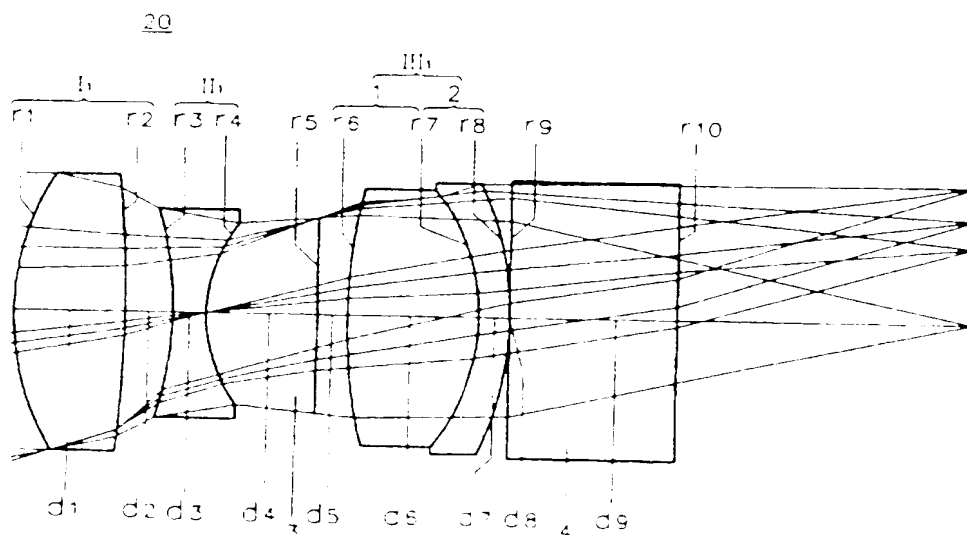
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(54) Telephoto and standard CCD camera lenses

(57) A telephoto-type lens system 20, of a head separated charge coupled device (CCD) camera, comprises a first lens group I₁ having a positive focal length, a second lens group II₁ having a negative focal length, and a third lens group III₁. The first lens group has a first convex lens surface facing an object and an upper convex surface. The third lens group has a second lens with a negative focal length joined to a first lens with a positive focal length. Iris diaphragm 3 and filter 4 are shown.

A standard type lens system (22, Fig 6) comprises a first negative lens group having two negative lenses, a second positive lens group and a third lens group having a negative lens followed by two positive lenses.

FIG. 1



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FIG. 1

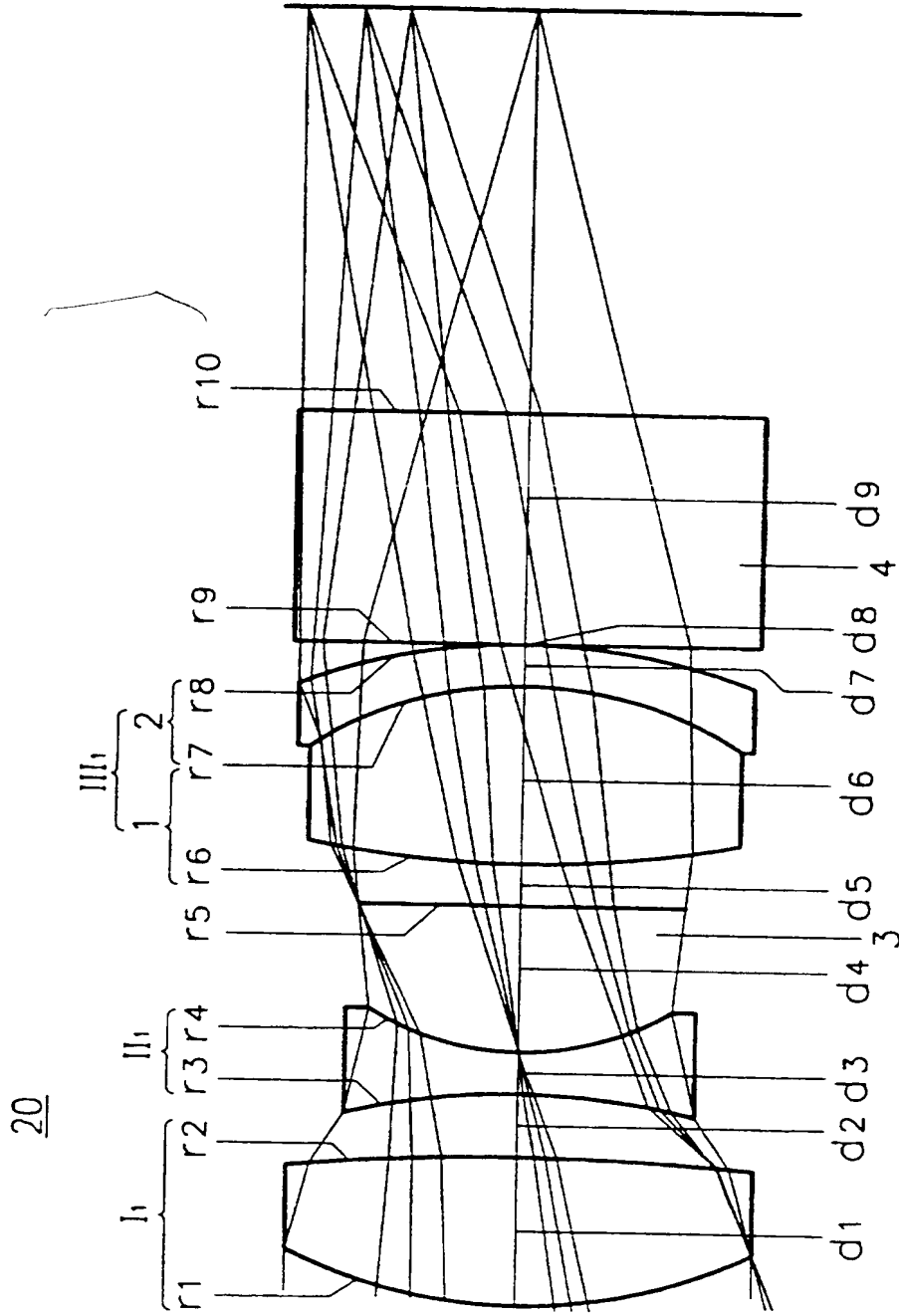


FIG.2

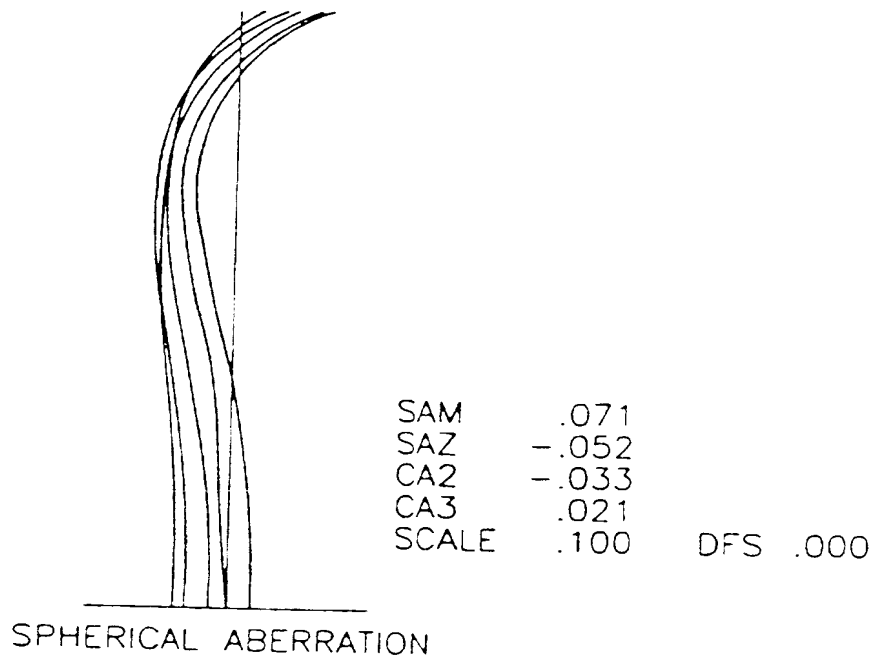


FIG.3

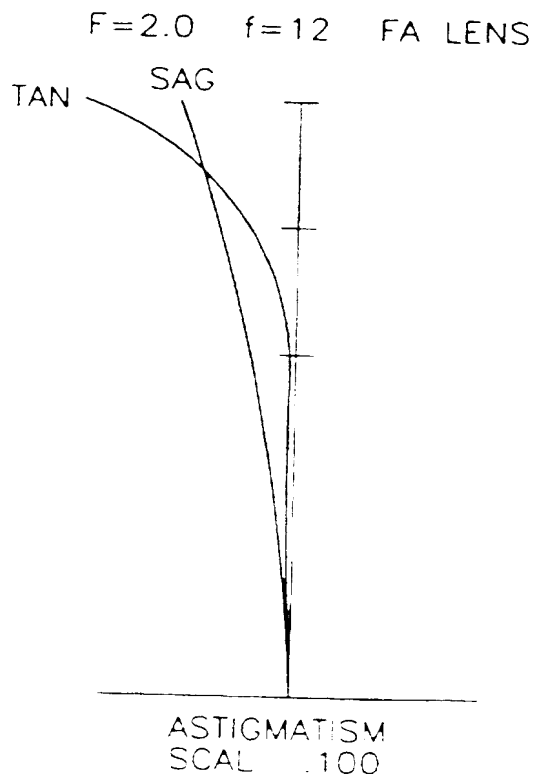


FIG.4

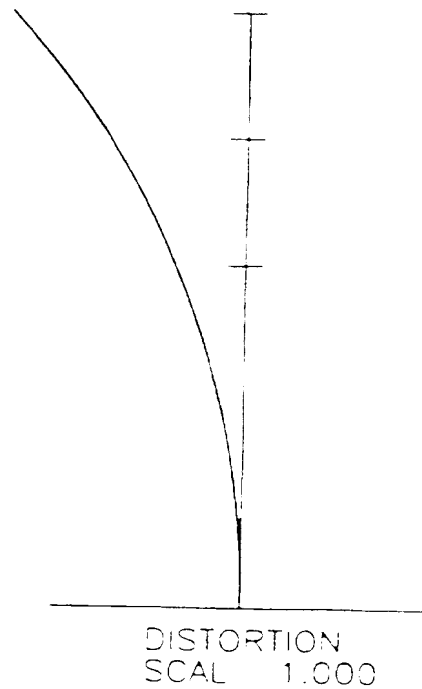


FIG.5

F=2.0 f=12 FA LENS

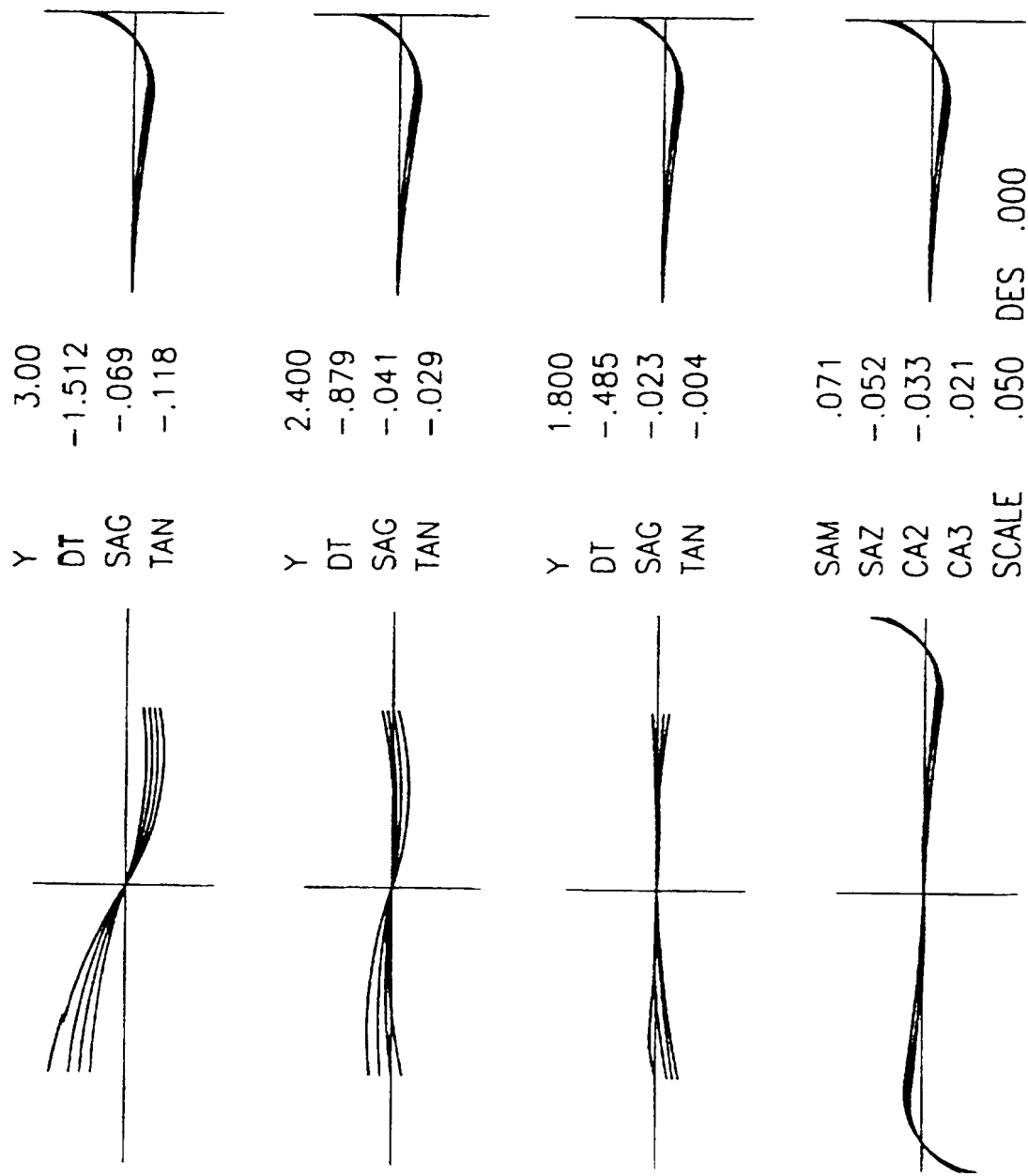


FIG.7

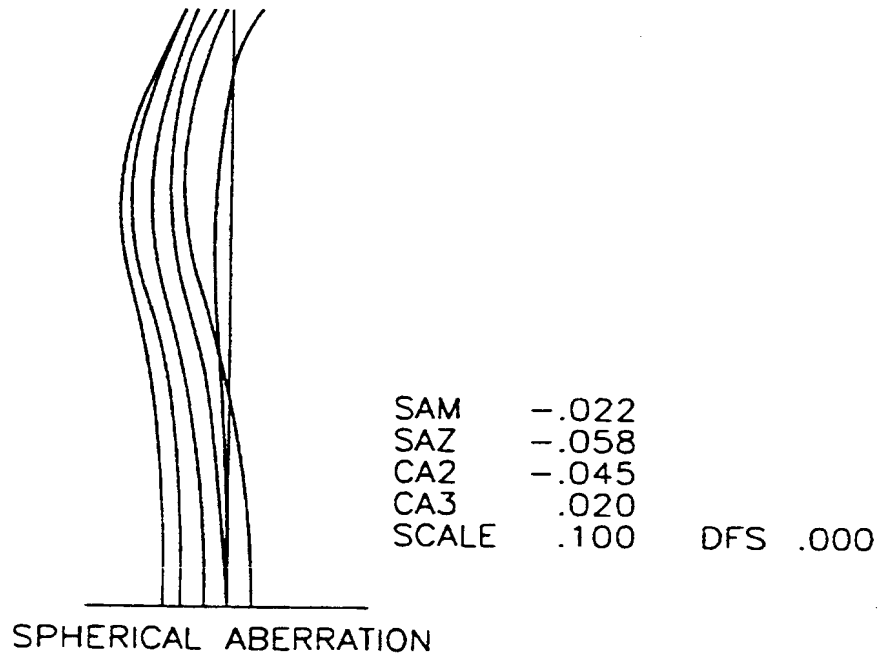


FIG.8

F=1.6 f=5.5 FA STANDARD LENS

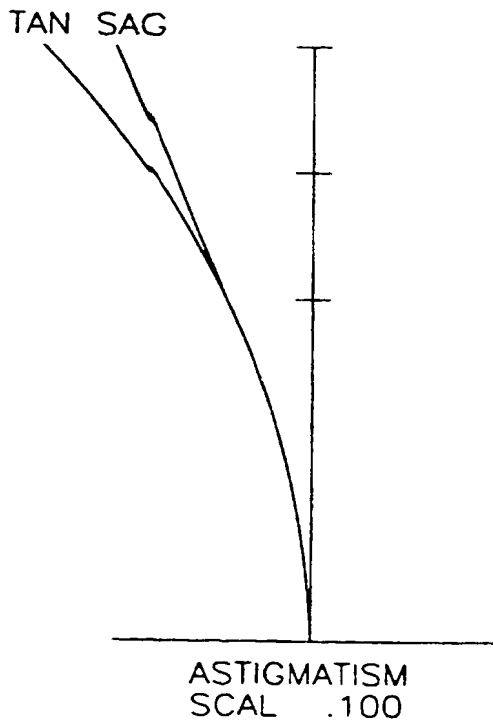


FIG.9

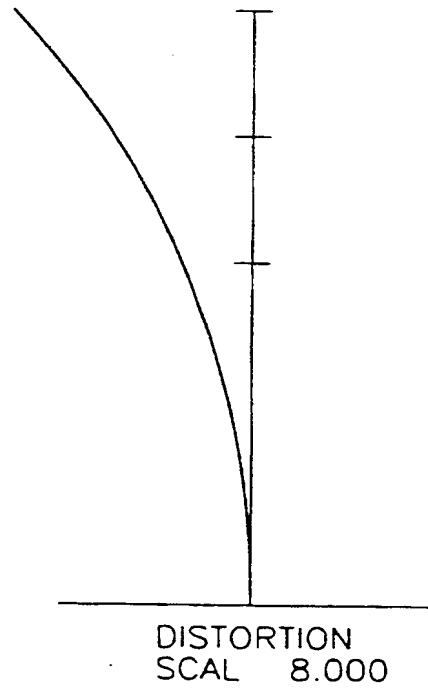
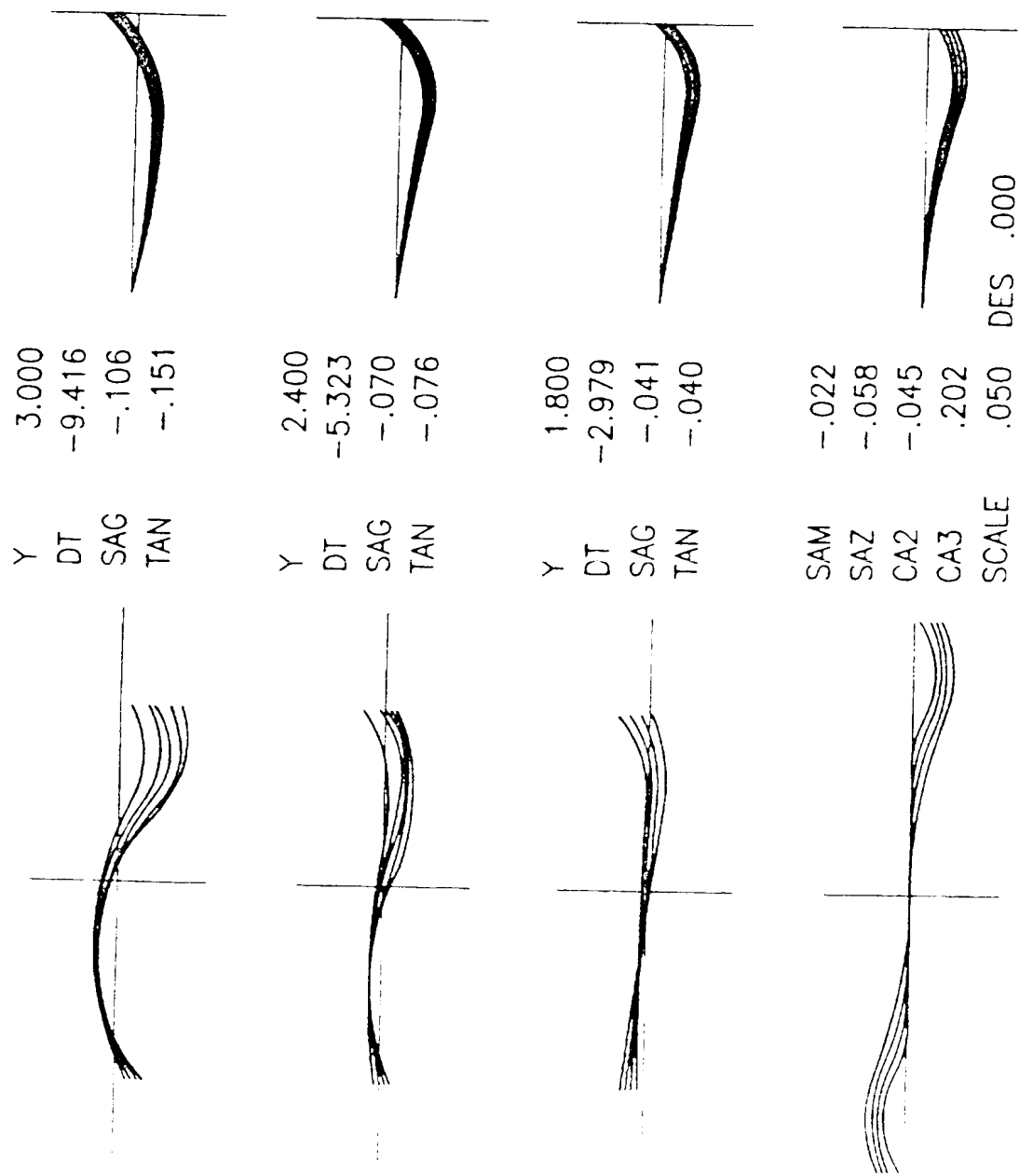


FIG.10

F=1.6 f=5.5 FA STANDARD LENS



LENS SYSTEM FOR A HEAD SEPARATED TYPE
CHARGE COUPLED DEVICE CAMERA

0 BACKGROUND OF THE INVENTION

Field of the Invention

This invention relates to a telephoto-type and standard-type lens system of a head separated charge coupled device (CCD) camera used for general monitoring.

5 Description of Prior Art

The lens system of a CCD camera typically uses optional lenses such as telescopic lenses, wide viewing angle lenses, etc. With CCD technology, it is possible to obtain high definition
10 images. The CCD camera has a lens mount for holding lenses. The typical mounts are C-mount and CS-mount, whereas the optional lenses are typically retro-focus type lenses.

The optical characteristics of retro-focus type lens are as follows: First, if the distortion aberration has a negative
15 value, it increases for a wide view angle lens with an image angle greater than 60°. Second, the back focal length increases, thereby making it difficult to obtain high definition by improving the aberration balance. Third, the retro-focus type lens system needs a highly refractive concave lens arranged at a
20 front position. This increases the absolute value of spherical aberration coefficient, which represents the difference between the central focal point of the lens center and the focal point of

a peripheral surface of the lens. Hence, there must be provided a means to correct the aberration in the rear portion.

These characteristics make it difficult to obtain a high definition CCD camera for use in factory automation (FA).

5 Moreover, a lens system satisfying the high definition requirements is not compact and light. To address such problems, the FA CCD camera employs a lens system designed to have an extremely small size and light weight. Additionally, CCD camera use in FA and vision system apparatus for checking the normal
10 operation of various machines is rapidly increasing. These apparatus include a head separated lens system that employs a connecting wire making it possible to separate the lens mount and the lens system.

15

SUMMARY OF THE INVENTION

Accordingly, it is an object of the present invention to provide a telephoto-type lens system of a FA CCD camera, which provides an image angle greater than 29° together with high definition.

20

It is another object of the present invention to provide a standard-type lens system of a head separated CCD camera, which provides an image angle greater than 63° together with high definition.

25

Additional objects and advantages of the invention will be set forth in part in the description which follows, and in part will be obvious from the description, or may be learned by

practice of the invention. The objects and advantages of the invention will be realized and attained by means of the elements and combinations particularly pointed out in the appended claims.

To achieve the objects and in accordance with the purpose of the invention, as embodied and broadly described herein, the invention comprises a telephoto-type lens system of a head separated charge coupled device (CCD) camera. The system includes a first lens group having a positive focal length, a second lens group having a negative focal length, and a third lens group. The first lens group has a first convex lens surface facing an object and an upper convex surface. The third lens group has a first lens having a positive focal length and a second lens having a negative focal length joined to the first lens.

According to another embodiment, the present invention comprises a standard-type lens system of a head separated CCD camera. The system includes a first lens group with a first and a second lens having a negative focal length, a second lens group having a positive focal length with both sides being convex, and a third lens group having a first, a second, and a third lens. The first lens of the first lens group has a first convex lens surface facing an object and an upper concave side with a negative focal length. The second lens of the first lens group has an upper concave side with a negative focal length. The first lens of the third lens group has a negative focal length with both sides being concave. The second lens of the third lens

group has a positive focal length with an upper convex side, and the third lens of the third lens group has a positive focal length with both sides being convex.

It is understood that both the foregoing general description
5 and the following detailed description are exemplary and exemplary only, and are not restrictive of the invention as claimed.

BRIEF DESCRIPTION OF THE DRAWINGS

The accompanying drawings, which are incorporated in and
10 constitute a part of the specification, illustrate a preferred embodiment of the invention. Together with the description, they serve to explain the objects, advantages, and principles of the invention. In the drawings:

Fig. 1 is a schematic diagram for illustrating the
15 construction of a telephoto type lens system of a CCD camera according to an embodiment of the present invention;

Fig. 2 is a graph for illustrating the spherical aberration of the lens system of Fig. 1;

Fig. 3 is a graphic for illustrating the astigmatic
20 aberration of the lens system of Fig. 1;

Fig. 4 is a graph for illustrating the distortion aberration of the lens system of Fig. 1;

Fig. 5 is the chromatic aberration of the lens system of Fig. 1;

Fig. 6 is a schematic diagram for illustrating the construction of a standard type lens system of a CCD camera according to a second embodiment of the present invention;

Fig. 7 is a graph for illustrating the spherical aberration of the lens system of Fig. 6;

Fig. 8 is a graphic for illustrating the astigmatic aberration of the lens system of Fig. 6;

Fig. 9 is a graph for illustrating the distortion aberration of the lens system of Fig. 6; and

Fig. 10 is the chromatic aberration of the lens system of Fig. 6.

DESCRIPTION OF PREFERRED EMBODIMENTS

Reference will now be made in detail to a telephoto-type lens system of a CCD camera according to the first embodiment of the present invention, as illustrated in Figs. 1-5.

The exemplary embodiment of a telephoto-type lens system of the present invention is shown in Fig. 1 and designated generally by reference numeral 20.

As embodied herein, and referring to Fig. 1, the telephoto-type lens system 20 includes a first lens group I1 having a first convex lens surface r_1 toward an object, an upper convex surface r_2 and a positive focal length. A second lens group II1 has a negative focal length toward the object. A third lens group III1 has a first lens 1 with a positive focal length and a second lens 2 with a negative focal length. An iris diaphragm 3 is between the second lens group II1 and the third lens group III1. A

limit, the distortion aberration rate increases. It is difficult to correct the aberration. Thus, the performance of the lens system is generally degraded. If the value falls below the lower limit, the correction of the aberration may be readily

5 accomplished. It becomes difficult, however, to secure the proper back focal length required to make a lens system used for both color and black/white.

The second formula (2) specifies the operatively allowable distance between the second lens group III1 and the iris diaphragm 10 3, and between the iris diaphragm 3 and the first lens 1 of the third lens group III1. In this case, if the value exceeds the upper limit, the operatively allowable distance of the iris diaphragm 3 is secured enough, but it becomes difficult to correct the aberration. If the value falls below the lower 15 limit, the correction of the aberration may be readily accomplished, thereby improving the performance of the lens system 20. It becomes quite difficult, however, to mount the iris diaphragm 3.

Further, the telephoto-type lens system of the present 20 embodiment satisfies the relationship defined by:

$$3.0 < \left[\sum_{I=1}^2 \frac{1}{F_{G3I}} \times \frac{1}{vd_{GI}} \times 10^2 \right] < 7.0 \text{ --- Formula (3)}$$

25 The symbol F_{G3I} represents the focal length of the "i"th lens of the third lens group III1 when numbered from the object side, and vd_{GI} the Abbe number of the above "i"th lens.

The formula (3) is used to correct the chromatic aberration, which is an optical lens defect causing color fringes because the lens material brings different colors of light to focus at different points. If the value deviates from the scope of the formula, a magnification chromatic aberration occurs in the upper part of the lenses out of the optical axis. It is especially difficult to correct the chromatic aberration of the g-line with a bluish color wavelength.

In addition, the inventive telephoto-type lens system of the head separated type CCD camera satisfies the relationship defined by:

$$80 < \left[\sum_{I=1}^9 \frac{1}{d_I} \times F \right] < 92 \quad \text{--- Formula (4)}$$

$$10 < \left[\sum_{I=1}^9 \frac{1}{d_I} \times F_b \right] < 15 \quad \text{--- Formula (5)}$$

The symbol d_I represents the central distance of the "i"th lens, F the combined focal length of the lens system 20, and F_b the back focal length of the lens system 20.

The formulas (4) and (5) are used to limit the whole length of the lens system and the length of the second lens group III. When these relationships are not satisfied, one cannot obtain a compact construction and readily correct aberration problems. Moreover, in this case, the back focal length is not secured,

thereby making it difficult to construct a lens system used for both color and black/white image.

Table 1 shows the characteristic values of the present embodiment when the lens number F_{NO} is 2.0, the combined focal length F 12.244, the back focal length F_b 5.8938, and the image angle W 28.83°. In Table 1, the reference symbol r_i ($i = 1, 2, \dots$) represents the radius of the curvature of each lens surface, d_i ($i = 1, 2, \dots$) the distance or thickness between two adjacent lens surfaces, nd_i the refractive index of each lens for wavelength "d", and vd_i the Abbe number of each lens for wavelength "d".

Table 1

Lens

| Surface No. | r | d | nd | vd |
|-------------|----------|------|---------|-------|
| 1 | 6.515 | 2.11 | 1.80420 | 46.50 |
| 2 | -85.420 | 1.09 | | |
| 3 | -11.5041 | 0.70 | 1.64769 | 33.84 |
| 4 | 4.259 | 2.14 | | |
| 5 | ∞ | 0.60 | 1.77250 | 49.62 |
| 6 | 17.147 | 2.55 | | |
| 7 | -4.988 | 0.7 | 1.80518 | 25.46 |
| 8 | -8.2180 | 0.0 | | |
| 9 | ∞ | 3.46 | 1.51680 | 64.20 |
| 10 | ∞ | | | |

0 Reference will now be made in detail to a standard-type lens system of a CCD camera according to the second embodiment of the present invention, as illustrated in Figs. 6-10.

 As embodied herein, and referring to Fig. 6, the standard type lens system 22 includes a first lens group I2, a second
5 lensgroup II2, and a third lens group III2. An iris diaphragm 24 is between the second lens group II2 and the third lens group III2. A filter 26 mounts behind the third lens group III2. The first lens group I2 includes a first lens Ia having a negative focal length with a first convex lens surface r1 facing toward
10 the object and the upper surface r2 being concave. A second lens Ib of the first lens group I2 has a negative focal length with the upper surface r4 being concave, thus producing the combined focal length as a negative value. The second lens group II2 has a positive focal length with the both sides r5, r6 being convex.
15 The third lens group III2 includes a first lens IIIa having a negative focal length with both sides r8, r9 being concave, a second lens IIIB having a positive focal length with the upper surface r11 being convex, and a third lens IIIC having a positive focal length with both sides r12, r13 being convex.

20 The present standard-type lens system of the present invention, as embodied herein, has a fixed focal length with three lens groups consisting of six lenses. The lens groups I2, II2, III2 have a negative, a positive, and a positive focal length, respectively. The first lens Ia of the first lens group
25 I2 is a concave lens (with respect to the object) having a

negative focal length, and the second lens has a positive focal length. The third lens group III2 includes a concave lens joined to a convex lens edge to edge and another convex lens behind them. In this way, the back focal length is secured enough to
5 satisfy the standard-type lens system of a head separated CCD camera used in factory automation (FA).

This standard-type lens system should satisfy the relationship defined by:

10
$$0.9 < \frac{F_b}{F} < 1.3 \text{ --- Formula (6)}$$

15
$$0.8 < \frac{d_7}{d_6} < 1.2 \text{ --- Formula (7)}$$

20 The symbol F represents the combined focal length of the lens system, Fb the back focal length, d6 the distance between the second lens group II2 and the iris diaphragm 24, and d7 the central distance between the iris diaphragm 24 and the first lens IIIa of the third lens group III2.

25 The formula (6) is used to specify the combined focal length and the back focal length, which makes it possible to produce a compact lens system. In this case, if the upper limit is exceeded, the distortion aberration increases. It is difficult to correct the aberration. Therefore, the performance of the
30 lens system is degraded. If the lower limit is exceeded, the correction of the aberration is readily accomplished. The back

focal length, however, is hard to secure for use in both color and black/white.

The formula (7) specifies the distance within the operating range for mounting the iris diaphragm 24 between the first lens group namely the first lens group I2 and the second lens group II2 and the rear lens group namely third lens group III2. In this case, when the upper limit is exceeded, the operational distance of the iris diaphragm 24 is secured enough, but correction of the aberration is hard to make. If the lower limit is exceeded, the correction of the aberration may be readily accomplished, thereby improving the performance of the lens system 22. It is difficult, however, to obtain the distance for mounting the iris diaphragm 24.

Further, the standard-type lens system of the present embodiment satisfies the relationship defined by:

$$0.1 < \left[\sum_{i=1}^2 \frac{1}{F_{Gi}} \times \frac{1}{vd_{Gi}} \times 10^2 \right] < -0.3 \quad \text{--- Formula (8)}$$

20

The symbol F_{Gi} represents the focal length of the "i"th lens of the first lens group numbered I2 from the object, and vd_{Gi} the Abbe number of the "i"th lens of the third lens group III2 numbered from the object.

The formula (8) is used to correct the chromatic aberration, which is an optical lens defect causing color fringes because the lens material brings different colors of light to focus at different points. If the value deviates from the scope of the

formula, a magnification chromatic aberration occurs in the upper part of the lenses out of the optical axis. It is especially difficult to correct the chromatic aberration of the g-line with a bluish color wavelength.

5 In addition, the inventive standard type lens system of the head separated type CCD camera satisfies the relationship defined by:

10
$$10 < \left[\sum_{I=1}^3 \frac{1}{d_I} \times F \right] < 20 \quad \text{--- Formula (9)}$$

15
$$80 < \left[\sum_{I=8}^{13} \frac{1}{d_I} \times F_b \right] < 100 \quad \text{--- Formula (10)}$$

20

The symbol d_I represents the central distance of the "i"th lens, F the combined focal length of the lens system 22, and F_b the back focal length of the lens system 22.

25 The formulas (9) and (10) are used to limit the whole length of the lens system 22 and the length of the second lens group II2. When these relationships are not satisfied, one cannot obtain a compact construction and readily correct aberration problems. Moreover, in this case, the back focal length is not
30 secured, thereby making it difficult to construct a lens system used for both color and black/white image.

Table 2 shows the characteristic values of the present embodiment when the lens number F_{NO} is 1.6, the combined focal

length F 5.5237, the back focal length F_b 5.7602, and the image angle W 63.31° . In Table 2, the reference symbol r_i ($i = 1, 2, \dots$) represents the radius of the curvature of each lens surface, d_i ($i = 1, 2, \dots$) the distance or thickness between two adjacent lens surfaces, nd_i the refractive index of each lens for wavelength " d ", and vd_i the Abbe number of each lens for wavelength " d ".

Table 2

Lens

| Surface No. | r | d | nd | vd |
|-------------|----------|------|---------|-------|
| I. | 11.410 | 1.30 | 1.48749 | 70.44 |
| II. | 4.635 | 1.26 | 1.51680 | 64.20 |
| III. | 27.311 | 0.60 | 1.84300 | 37.34 |
| IV. | 5.257 | 3.25 | 1.84666 | 23.73 |
| V. | 12.625 | 2.19 | 1.62041 | 60.34 |
| VI. | -16.994 | 2.01 | 1.58913 | 61.25 |
| VII. | ∞ | 1.91 | | |
| VIII. | -16.7220 | 0.70 | | |
| IX. | 10.376 | 0.24 | | |
| X. | 32.133 | 1.94 | | |
| XI. | -6.825 | 0.10 | | |
| XII. | 9.282 | 2.30 | | |
| XIII. | -15.452 | 0.00 | | |
| XIV. | ∞ | 3.46 | | |
| XV. | ∞ | | | |

0 Thus, there is provided the standard-type lens system for
the head separated CCD camera, which has the image angle greater
than 69° and produces high definition images. Also provided is
the telephoto type lens system having tessa type lens groups,
which has the image angle greater than 29° and produces high
5 definition images.

Other embodiments of the invention will be apparent to those
skilled in the art from consideration of the specification and
practice of the invention disclosed herein. It is intended that
the specification be considered as exemplary only, with a true
10 scope and spirit being indicated by the following claims.

CLAIMS

1. A telephoto-type lens system of a head separated charge coupled device (CCD) camera, comprising:

a first lens group having a positive focal length, the first lens group having a first convex lens surface facing an object and an upper convex surface;

a third lens group having a first lens having a positive focal length and a second lens having a negative focal length joined to a first lens, the first lens being oriented closer than the second lens to the first lens group; and

a second lens group having a negative focal length disposed between the first lens group and the third lens group.

2. The system of Claim 1, satisfying the relationships defined by:

$$0.3 < \frac{F_b}{F} < 0.6$$

$$0.2 < \frac{d_5}{d_4} < 0.5$$

wherein F represents a combined focal length of the lens system, F_b the back focal length, d_4 the distance between the second lens group and an iris diaphragm disposed between the second lens group and the third lens group, and d_5 the central distance between the iris diaphragm and the first lens of the third lens group.

3. The system of Claim 1, satisfying the relationships defined by:

$$3.0 < \left[\sum_{I=1}^2 \frac{1}{F_{G3I}} \times \frac{1}{vd_{GI}} \times 10^2 \right] < 7.0$$

wherein F_{G3I} represents the focal length of the "i"th lens of the third lens group when numbered from the object side, and vd_{GI} the Abbe number of the above "i"th lens.

4. The system of Claim 1, satisfying the relationship defined by:

$$80 < \left[\sum_{I=1}^9 \frac{1}{d_I} \times F \right] < 92$$

$$10 < \left[\sum_{I=1}^9 \frac{1}{d_I} \times Fb \right] < 15$$

wherein d_I represents the central distance of the "i"th lens, F the combined focal length of the lens system, and Fb the back focal length of the lens system.

5. A standard-type lens system of a head separated CCD camera, comprising:

a first lens group with a first and a second lens having a negative focal length, the first lens of the first lens group having a first convex lens surface facing an object and an upper concave surface with a negative focal length, the second lens of the first lens group disposed further from the object than the first lens, the second lens having an upper concave side with a negative focal length;

a third lens group having a first, a second, and a third lens, the first lens of the third lens group having a negative focal length with both sides being concave, the second lens of the third lens group having a positive focal length with an upper convex side, and the third lens of the third lens group having a positive focal length with both sides being convex, the second lens being between the first lens and the third lens, the first lens oriented closer than the second lens to the first lens group; and

a second lens group having a positive focal length with both sides being convex, the second lens group being between the first lens group and the third lens group.

6. The system of Claim 5, satisfying the relationship defined by:

$$0.9 < \frac{F_b}{F} < 1.3$$

$$0.8 < \frac{d_7}{d_6} < 1.2$$

wherein F represents the combined focal length of the lens system, F_b the back focal length, d_6 the distance between the second lens group and the iris diaphragm disposed between the second lens group and the third lens group, and d_7 the central distance between the iris diaphragm and the first lens of the third lens

group.

7. The system of Claim 5, satisfying the relationship defined by:

$$0.1 < \left[\sum_{I=1}^2 \frac{1}{F_{GI}} \times \frac{1}{vd_{GI}} \times 10^2 \right] < -0.3$$

wherein F_{GI} represents the focal length of the "i"th lens of the first lens group numbered from the object, and vd_{GI} the Abbe number of the "i"th lens of the third lens group numbered from the object.

8. The system of Claim 5, satisfying the relationship defined by:

$$10 < \left[\sum_{I=1}^3 \frac{1}{d_I} \times F \right] < 20$$

$$80 < \left[\sum_{I=8}^{13} \frac{1}{d_I} \times F_b \right] < 100$$

wherein d_I represents the central distance of the "i"th lens, F the combined focal length of the lens system, and F_b the back focal length of the lens system.

9. A telephoto-type lens system of a head separated charge coupled device camera, substantially as herein described with reference to the accompanying drawings.

Patents Act 1977
 Examiner's report to the Comptroller under Section 17
 (The Search report)

20

Application number
 GB 9600012.0

Relevant Technical Fields

- (i) UK Cl (Ed.O) G2J (JB7CX)
 (ii) Int Cl (Ed.6) G02B

Search Examiner
 MR C ROSS

Date of completion of Search
 6 MARCH 1996

Databases (see below)

(i) UK Patent Office collections of GB, EP, WO and US patent specifications.

Documents considered relevant following a search in respect of Claims :-
 1-4

(ii)

Categories of documents

- X: Document indicating lack of novelty or of inventive step
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 A: Document indicating technological background and/or state of the art.
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 E: Patent document published on or after, but with priority date earlier than, the filing date of the present application.
 &: Member of the same patent family, corresponding document.

| Category | Identity of document and relevant passages | | Relevant to claim(s) |
|----------|--|--------------------------------|----------------------|
| X | GB 2225123 A | (ASAHI) | 1 at least |
| X | GB 0609408 | (T, T & H) see Examples I, III | 1 at least |
| X | US 5073017 | (CANON) see Figure 2 | 1 at least |
| X | US 4732459 | (NIPPON KOGAKU) see Figure 3 | 1 at least |
| X | US 4518229 | (MINOLTA) | 1 at least |
| X | US 4483597 | (OLYMPUS) see Figure 4 | 1 at least |
| X | US 4251133 | (CANON) | 1 at least |
| X | US 4241983 | (CANON) | 1 at least |
| X | US 4240703 | (CANON) | 1 at least |
| X | US 4176913 | (NIPPON KOGAKU) | 1 at least |
| X | US 4063802 | (OLYMPUS) | 1 at least |
| X | US 4045128 | (CANON) see Table 1 | 1 at least |
| X | US 3848972 | (OLYMPUS) | 1 at least |

Databases: The UK Patent Office database comprises classified collections of GB, EP, WO and US patent specifications as outlined periodically in the Official Journal (Patents). The on line databases considered for search are also listed periodically in the Official Journal (Patents).

